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Overtopping

(low head

water turbine)

FRAMEWORK AND AIMS

Oscillating Water Column (air turbine)



CONSOLIDATED

BUT....

Oscillating body

(hydraulic motor, hydraulic turbine, linear electric generator)



(Classification as in Falcão, 2010)

Research is still needed to maximize conversion efficiency & survivability/operability in severe wave conditions OWC could have limited operability in energetic sea-states (efficiency loss/ damage at air turbine for excessive air pressure).

Relief valve are sometimes used to regulate excessive air chamber pressure (*Falcão & Justino, 1999; Falcão et al., 2003*).





FRAMEWORK AND AIMS

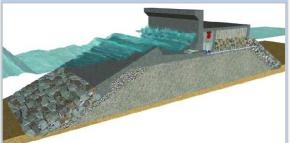
Oscillating Water Column (air turbine)

Oscillating body (hydraulic motor, hydraulic turbine, linear electric generator)



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Overtopping (low head water turbine)

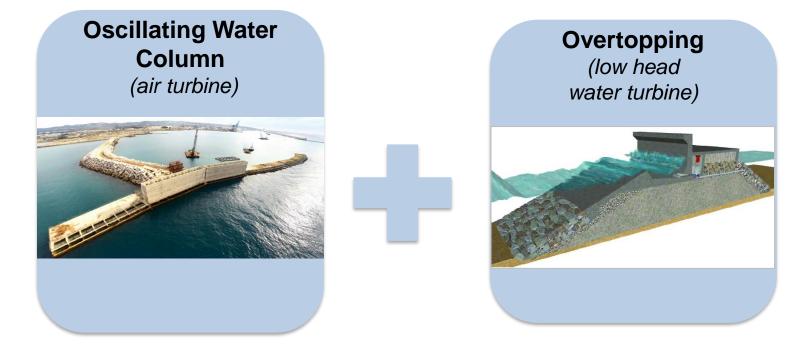


- The stored potential energy is used to activate a low head hydraulic turbine.
- Recognized advantages: (i) possibility to store the wave energy;
 (ii) the low head hydraulic turbine is a consolidated technology.
- BUT... Wave overtopping takes place just in case of relatively high energetic sea-states.





FRAMEWORK AND AIMS



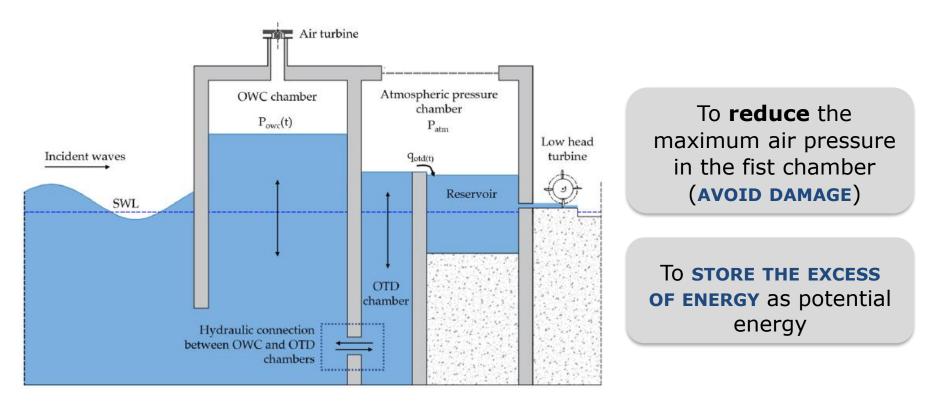
- A Hybrid OWC-OTD device referred to as Oscillating and Overtopping Water Column (O²WC) wave energy is proposed
- □ Particularly suitable for breakwater integration
- □ Its functioning is studied by means of laboratory tests





THE O-OWC CONCEPT

- First chamber: OWC chamber equipped with an air turbine for PTO, connected to the second chamber through underwater apertures
- Second chamber at atmospheric pressure: when the free surface exceeds the freeboard, water overtops into a reservoir (potential energy storage)

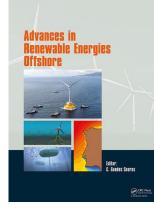






MDPI

THE O-OWC CONCEPT



Advances in Renewable Energies Offshore – Guedes Soares (Ed.) © 2019 Taylor & Francis Group, London, ISBN 978-1-138-58535-5

Laboratory tests on an original wave energy converter combining oscillating water column and overtopping devices

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Marine Technology and Ocean Engineering Series Volume 10 Trends in Renewable Energies Offshore



Chapter

Development of a hybrid oscillating water column-overtopping device: Preliminary results of laboratory tests at scale 1:25 on the O2WC WEC By I. Simonetti, A. Esposito, L. Cappietti



rticle

Experimental Proof-of-Concept of a Hybrid Wave Energy Converter Based on Oscillating Water Column and Overtopping Mechanisms

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THE SMALL-SCALE MODEL OF THE DEVICE



2D model

Froude scaling Scale 1:25 □ Width of the model: **B** =79cm

- Slot to reproduce the PTO damping
- Submerged opening connecting OWC and overtopping chambers: variable size G
- □ Overtopping into a reservoir \rightarrow measured

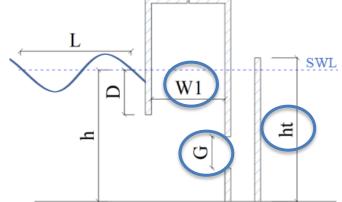




THE SMALL-SCALE MODEL OF THE DEVICE

Geometry parameters tested:

- □ OWC chamber width W1=0.33 m → W1/L between 0.068 and 0.22
- Submerged opening of variable size (G=0-10 cm, with a step of 2 cm).
- 3 values of the overtopping threshold in the second chamber (ht=0.61 - 0.65 cm)



□ Top cover slot: 1.6% of top cover area

Wave	ve scale 1:25			
code	н	т	L	steepnes
H01	0.08	1	1.54	0.078
H02	0.08	1.2	2.12	0.057
H03	0.08	1.4	2.33	0.052
H04	0.08	1.6	3.25	0.037
H16	0.16	1.8	3.79	0.042
H17	0.16	2	4.33	0.037

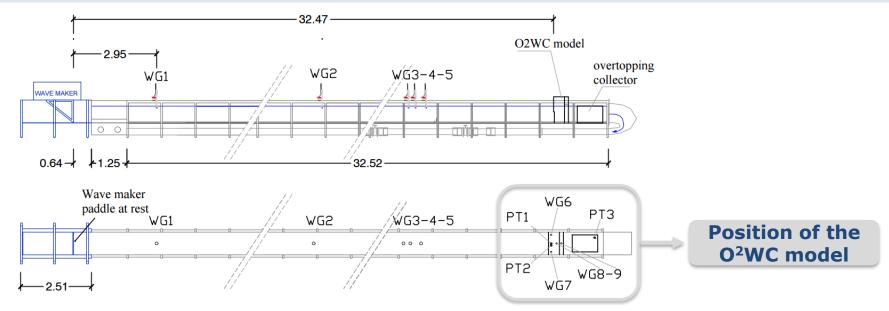
Test conditions:

- regular waves only
- Wave heights varying between 0.08 and 0.16 m (**2-4 m** at full scale) and periods in the range 1-2 s (5-10 s at full scale)
- water depth h=0.59m





CURRENT-WAVE FLUME SET-UP



- □ 9 ultrasonic distance sensors WG, accuracy ±1mm
- □ WG6, WG7, WG8 to measure the water level in the OWC chamber, WG9 to measure the level in the overtopping chamber
- □ 2 **Pressure Transducer PT** (full scale 100mBar & accuracy ±0.1%FS) for pressure variations in the OWC chamber
- □ 1 **PT** to measure the water level in the overtopping reservoir
- 200 Hz acquisition frequency





ESTIMATION OF THE CAPTURE WIDTH

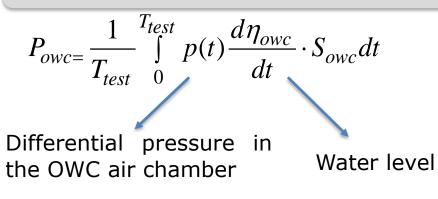
$$P_{wave} = \frac{1}{16} \rho g H^2 \frac{\omega}{k} \left(1 + \frac{2kh}{\sinh(2kh)} \right)$$

Period averaged incident wave power [W/m]

$$CW = \frac{P_{extracted}}{P_{wave} \cdot B} = \frac{(P_{owc} + P_{otd})}{P_{wave} \cdot B} = CW_I + CW_{II}$$

Device width

Power extracted as pneumatic power (air flux) in the first chamber:



Hydraulic power of the flow overtopped from the second chamber

$$P_{odt} = q_{otd} \cdot \Delta h_{otd} \cdot \rho \cdot g$$

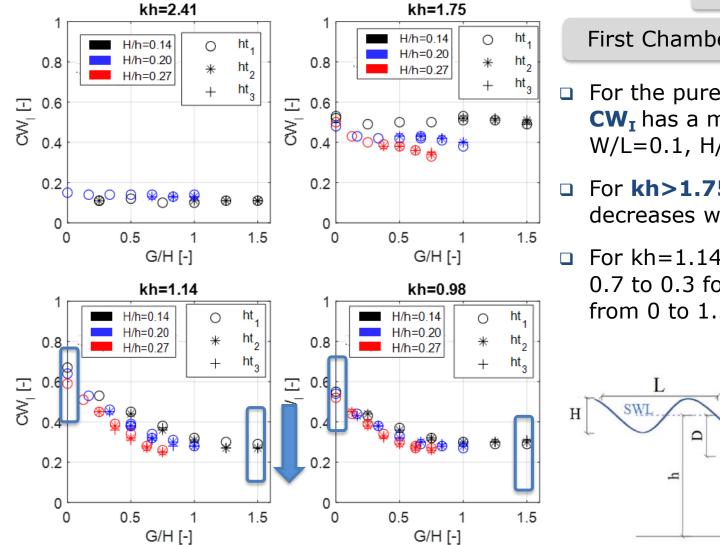
Hydraulic head

Average flow discharge from the second chamber

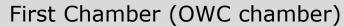




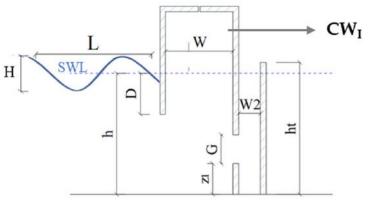
RESULTS



CWI



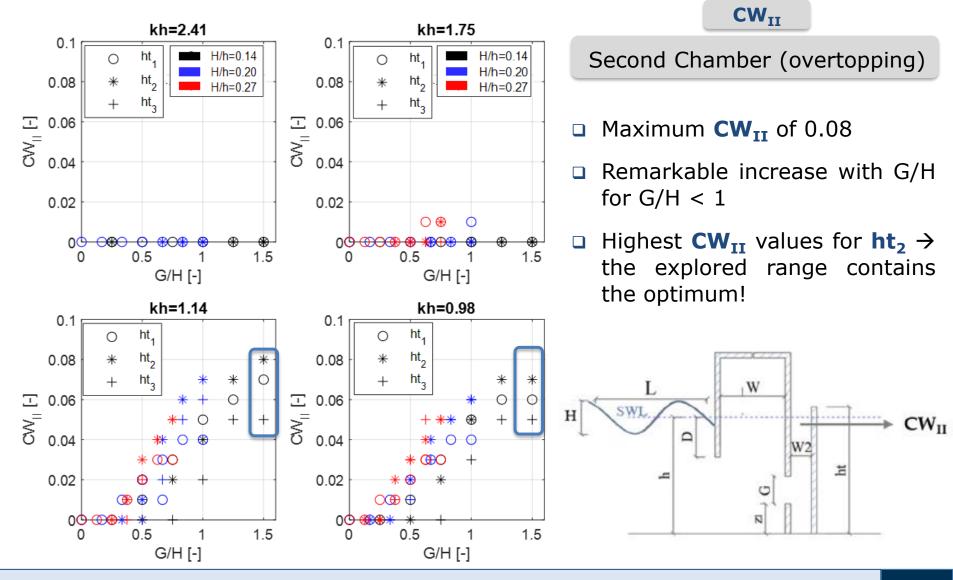
- For the pure OWC case (G/H=0),
 CW_I has a maximum of 0.7 (for W/L=0.1, H/h=0.14)
- For kh>1.75, CW_I remarkably decreases when increasing G/H
- For kh=1.14, CW_I decrease from 0.7 to 0.3 for G/H increasing from 0 to 1.5







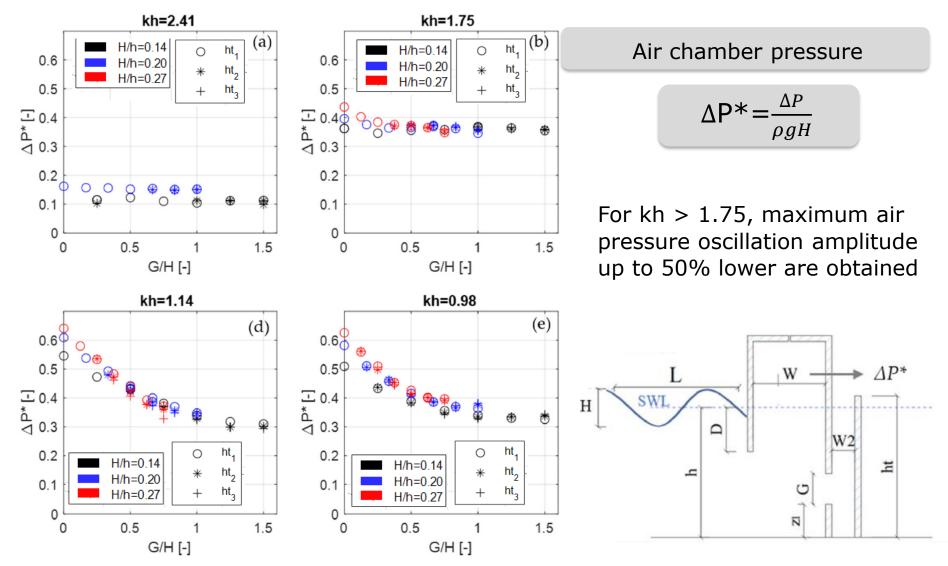
RESULTS







RESULTS



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CONCLUSIONS

Laboratory tests

Adding the OTD device to the OWC device can be useful to **limit the maximum air pressure in the OWC chamber**, aiding to implement strategies for **safe functioning of the air turbine**

The decrease of CW_I resulting from the lower air pressure **can be only partially recovered** by the additional CW_{II} in the OTD chamber

Results can be used for calibration/validation of **numerical models** for further optimization of the concept

Outlooks

The present results are limited to the primary efficiency, to fully asses the potentiality of the device in terms of energy extraction, further studies including the PTO are fundamental (e.g. the maximum air pressure/air flowrates are strongly turbine-specific) \rightarrow wave-to-wire models





THANKS FOR YOUR ATTENTION

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